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Research Article

Evaluation of Controlled Release Theophylline Microspheres Prepared with Cellulose Acetate Using Solvent Evaporation Method

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Abstract

Purpose: To formulate theophylline microspheres with cellulose acetate using solvent evaporation method and evaluate the effect of various processing factors on their characteristics.

Methods: Microspheres containing the phylline were prepared with a hydrophilic, biocompatible polymer - cellulose acetate - by an emulsion solvent evaporation technique using an acetone/liquid paraffin system containing Span 80 as a surfactant. The effect of processing factors, e.g., varying drug/polymer ratio (1:1, 1:2, 1:3) and temperature (10 and 35 °C) on microsphere characteristics and drug release were examined. Similarly, microspheres with a drug/polymer ratio of 1:3 incorporating Span 20 were also also prepared and evaluated.

Results: The microspheres were white, free-flowing and spherical. The yield varied from 73.0 to 87.5 % while entrapment efficiency was in the region of 71.8 to 92.4 %. High drug/polymer ratio, Span 80 (surfactant) and processing temperature between 10 and 30 °C produced formulations with better drug entrapment efficiency. High drug/polymer ratio, low processing temperature and low HLB value of surfactant enhanced the sustained drug release characteristics of the microspheres.

Conclusion: The combination of three suitable factors - Span mixture (with HLB value of 4.3), processing temperature of 10 $^{\circ}$ C and drug/polymer ratio of 1:3 - produced a suitable controlled release theophilline microsphere formulation which could be effective for the management of asthma.

Keywords: Microsphere, Emulsion solvent evaporation, Theophylline, Temperature, HLB value.

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INTRODUCTION

The microencapsulation technique by solvent evaporation process has been extensively studied in recent years for the preparation of microspheres. This is a complex process and requires strict control of several processing parameters such as rate of solvent evaporation, stirrina rate. viscositv of polymeric phase, drug polymer ratio, volume ratio between inner phase and outer phase and amount of surfactant, in order to develop a therapeutically effective dosage form [1].

Some studies have been carried out earlier using polymethacrylate polymers (Eudragit RS 100, RSPO, etc) and dextran regarding the effect of processing temperature on microsphere characteristics [1,2] but no work has been reported, to the best of our knowledge, on the effect of processing temperature and Span HLB value on cellulose acetate microsphere formulation and release characteristics. The role of temperature in emulsion solvent evaporation process is a matter of great significance since it affects the rate and way at which the organic solvent is removed from the microspheres and ultimately, the shape, size, and drug loading efficiency [1].

Surface active agents play a significant role in microsphere formulation by emulsification solvent evaporation method. They have the properties of adsorbing to the interface and stabilizing the emulsion droplets bv preventing their aggregation. Cellulose acetate (CA) the acetate ester of cellulose is a biocompatible hydrophilic polymer and has been used as a microencapsulating agent in several studies [2-4]. Theophylline (TH), the drug of choice for the treatment of asthma has a short elimination half-life, and its toxicity is dose-dependent. All the side effects can be controlled efficiently if the drug is administered controlled as а release formulation [5].

To the best of our knowledge, the effect of process parameters such as temperature and

hydrophilic/lipophilic balance (HLB) value of surfactant on characteristics of theophylline (TH) microspheres prepared with cellulose acetate (CA) has not been carried out. Therefore, the objective of this study was to evaluate the effect of drug/polymer ratio, process temperature and surfactant HLB value on the shape, size, flow property, drugloading efficiency and drua release characteristics of theophylline CA microspheres prepared by solvent evaporation method using acetone/liquid paraffin system, as well as determine the potentially most suitable controlled release formulation for asthma management

EXPERIMENTAL

Materials

Theophylline (TH) and cellulose acetate (CA) were obtained as gifts from Macleod, Mumbai, India, while Span 20 and 80 were procured from Central Drug House (P) Ltd, New Delhi, India. All other reagents and solvents used were of pharmaceutical or analytical grade.

Method of preparation

Cellulose acetate (CA), ranging from 0.25 to 0.75 g, was dissolved in 10 ml of acetone and 0.25 g of theophylline (the fraction passing through a sieve with aperture size of 36 µm) was suspended in the CA solution and stirred with a magnetic stirrer. The resultant dispersion was poured into 100 ml of light liquid paraffin, containing 1.5 %w/v of Span 80 (HLB value 4.3) as an emulsifying agent, in a 250 ml beaker which was rotated in a water bath at 600 rpm at 30 ℃ for 7 h. The resulting microspheres were filtered through a Whatman filter paper no. 1. The residue was washed 4 - 5 times in 50 ml n-hexane on each occasion. The microspheres were dried at room temperature for 24 h [6.7]. Microspheres with varying drug/polymer ratio (1:1, 1:2, 1:3) were coded F1, F2 and F3, respectively. **Microspheres** were also prepared with a drug/polymer ratio of 1:3 using Span 80 (HLB value, 4.3) at 10 and 35 °C and denoted F4 and F5, respectively. Similarly, microspheres with a drug/polymer ratio of 1:3 using Span 20 (HLB value, 8.6) at a temperature of 30 °C was denoted F6.

Determination of microsphere yield

The microspheres were weighed and the yield of microspheres was calculated using Eq 1.

Yield $(\%) = (A/B) \times 100$ (1) where A is the weight of microspheres obtained and B is the theoretically expected weight of microspheres.

Assessment of size distribution of microspheres

The microspheres were separated into different size fractions by sieving for 10 min using a mechanical sieve shaker (Cuprit Electrical Co., India) containing standard sieves with apertures of 710, 500, 355, 250 and 180 μ m, respectively. The particle size distribution of each of the microsphere batch was determined [7] and their mean particle size calculated using Eq 2.

Mean particle size = Σ (P x W)/ Σ W(2) where P is the mean particle size of the fraction and W is the weight of the fraction.

Micromeritic studies

The flow properties of the microspheres were evaluated by determining Carr's index [7] as in Eq 3.

Carr's index = $\{(TD - BD) \times 100\}/TD \dots$ (3) where TD is tapped density and BD bulk density. The bulk and tapped densities were measured in a 10 ml graduated measuring cylinder.

Surface accumulation studies

This study was conducted to estimate the amount of drug present on the surface of the microspheres. An accurately weighed quantity of the microspheres (50 mg) was

suspended in 50 ml of phosphate buffer (pH 6.8) and agitated on a mechanical shaker for 15 min. The amount of drug leached from the surface of the microspheres was analyzed spectrophotometrically using Systronic 2101 UV–Visible spectrophotometer at 271 nm and expressed as a proportion of the entrapped drug in the microspheres [9].

Drug entrapment efficiency

accurately weighed About 50 mg of microspheres were added to 50 ml of phosphate buffer, (pH 6.8) and then agitated on a mechanical shaker for 24 h. The mixture was filtered with Whatman membrane filter, BA85 grade (0.45 µm pore size) and, after suitable dilution, analyzed spectrophotometrically at 271 nm using Systronic 2101 UV Visible spectrophotometer.

Scanning electron microscopy (SEM)

A scanning electron microscope (JEOL JSM -5200) was used to characterize the surface topography of the microspheres at 20 kV. Prior to examination the microspheres were fixed on a metallic support with a thin adhesive tape and microspheres were coated with gold under vacuum (fine coat, ion sputter JFC -1110) to render them electron conductive.

In vitro release studies

In vitro release studies on the microspheres (355 µm fraction) were carried out at 37 °C in 500 ml 0.1M HCl (pH 1.2) for the first 2 h and then in 500 ml phosphate buffer (pH 6.8) in a USP basket type dissolution test apparatus Disso-2000. (Labindia. Mumbai. India) rotated at 100 rpm. At preset time intervals, 2 ml aliquots were withdrawn and replaced by an equal volume of fresh dissolution medium. The withdrawn samples were filtered (0.45 µm pore size) and, after suitable dilution, analyzed spectophotometrically at 271 nm. Each test was carried out in triplicate.

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Batch code	Yield (%)	Carr's index	Mean particle size (µm)	Surface drug (%)	Encapsulation efficiency %
*F1	85.3±4.7	8.81	463±2.6	3.6±0.0.2	78.6±1.3
*F2	85.4±2.6	7.38	521±4.4	2.1±0.3	86.2±2.0
*F3	78.5±1.5	4.94	608±2.0	1.2±0.1	90.9±1.8
**F4	85.2±2.2	5.22	386±3.6	1.4±0.2	93.4±0.9
***F5	87.5±1.0	9.90	731±2.0	4.0±0.3	71.8±1.2
[°] F6	72.9±2.6	5.38	747±0.6	12.0±0.5	79.1±2.4

Table 1: Some of the	characteristics of	the microspheres	(+SD.	n = 3)
			$(\pm 0D)$	

*Formulations containing drug/polymer ratio of 1:1, 1:2, 1:3 incorporating Span 80 and prepared at 30 °C, are denoted F1, F2 and F3, respectively; F4 contain drug/polymer ratio 1:3, Span 80 and prepared at 10 °C; F5 and F6 contains drug/polymer ratio 1:3, Span 80, and prepared at 35 and 30 °C, respectively

Statistical analysis

The quantitative data were expressed as mean ± standard deviation (SD), and statistical analysist on the data were performed using one-way ANOVA (Graph Pad Prism 5). Differences between formulations were considered to be significant at $p \le 0.05$.

RESULTS

Characteristics of microspheres

The microspheres were white, free-flowing and spherical. The yield varied from 72 - 85 %. The quantitative characteristics of the microspheres are shown in Table 1. Carr's index, which is a measure of flow property, was < 10 for all the formulations suggesting that they possessed excellent flow properties [10]. Higher polymer/drug ratio, processing temperature and surfactant HLB value of Span lead to increase in the mean particle size of microspheres. The entrapment efficiency of the various microspheres was in the range 70.8 to 92.4 %. Formulation F3 had higher drug loading than F6 ($p \le 0.05$). Higher polymer/drug ratio, Span 80 and processing temperature of 10 and 30 ℃ favoured higher drug entrapment.

Scanning electron microscopy (SEM)

The SEMs of the microspheres are displayed in Fig 1 with Fig 1A (F4) showing the general

appearance of the microspheres. F3 (Fig 1B) had a smooth surface without visible evidence of drug particles on its surface while F6 (Fig 1C) shows the presence of drug particles on the microsphere surface. Fig 1D (SEM of F5) indicate some holes and fractures on the surface.



Fig 1: SEM photomicrographs of some microsphere formulations: (A) = F4(X 50); (B) = F3(X 200); (C) = F6(X 50), and shows the presence of drug particles on microsphere surface; and (D) = F5(X 200), and shows holes and fractures on microsphere surface

In vitro drug release

Higher polymer/drug ratio, lower processing temperature and low HLB value of Span had an elevated effect on the sustained release characteristics of the microspheres.



Fig 2: Effect of drug/polymer ratio on drug release from microsphere formulations F1 (\bullet), F2 (\circ), and F3 (\blacktriangle).



Fig 3: Effect of processing temperature on drug release from microsphere formulations F3 (\Box), F4 (\bullet), and F5 (\blacktriangle)



Fig 4: Effect of HLB value of Span on drug release from microsphere formulations F3 (\blacksquare) F3 and F6 (Δ).

DISCUSSION

Microsphere size

The increase in particle size of the microspheres with increase in polymer/drug ratio was due to the fact that the viscosity of the dispersed phase increased with increase in polymer/drug ratio, resulting in larger emulsion droplets which were difficult to break and, precipitated to become the microspheres [10]. Increase in temperature from 10 to 35 °C favoured formation of larger microspheres and this may be explained by the likelihood that at the lower temperature, when the polymeric phase was added to the oil phase and stirred, extensive emulsification of the polymeric phase occurred with the solvent in the polymeric phase diffusing into the outer oil phase, and evaporating from the system, and thus resulting in small-size microparticles. However, the higher temperature increased the rate of solvent evaporation with the emulsion droplets hardening faster and the stirrer shear force unable to break the droplets, thus leading to formation of larger particles [1,6].

The surfactant type used also affected particle size as Span 80 (HLB value, 4.3) resulted in the formation of comparatively smaller particle than Span 20 (HLB value, 8.6). This may be due to better stabilization of the emulsified droplets at the lower HLB value as Span 20 may have facilitated collision of small emulsified droplets to form larger particles.

Drug entrapment

The increase in drug entrapment efficiency with increase in polymer/drug ratio may be attributed to increase in polymer viscosity with the result that the microsphere hinders escape of the entrapped drug. Formulations F3 and F4 showed > 90 % entrapment efficiency, suggesting that process temperatures \leq 30 °C had no effect on drug entrapment. However, at 35 °C, increased solvent evaporation created holes and fractures in the microsphere (F5, Fig 1D). These flaws constituted channels for the escape of the entrapped drug into the processing medium, leading to low drug entrapment.

Drug release

As polymer/drug ratio increased, drug release became more sustained because the polymeric phase became more viscous and this, in turn, strongly shielded the drug and hampered the diffusion of the dissolution medium into microsphere core to dissolve the drug as well as the diffusion of the dissolved drug out of the microsphere [11-13]. Lower processing temperature reduced the rate of drug release from the microspheres.

The photomicrographs indicate that while the microspheres formulated at 10 °C had no holes on their surfaces, those formulated at 30 and 35 °C showed the presence of either holes or holes plus fractures on their surfaces. These flaws probably acted as channels for the dissolution medium to access the core of the microspheres as well as diffusion of the dissolved drug from the microspheres.

Formulation F6 released drug in a faster manner than F3 due probably to the higher HLB value of Span 80 which facilitated the formation of a more stable microsphere with a greater capacity to retard drug diffusion than the microspheres (F3) prepared with Span 20 as the emulsifying agent.

CONCLUSION

Formulation F4, which combined three optimized process factors, namely, Span 80 (HLB value, 4.3), processing temperature of 10 °C and drug/polymer ratio 1:3, yielded the satisfactory sustained theophylline release formulation of all the formulations evaluated

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