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Research Article

Compression, Mechanical and Release Properties of Chloroquine Phosphate Tablets containing corn and Trifoliate Yam Starches as Binders

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Abstract

Purpose: A study was made of the binding properties of trifoliate yam starch, obtained from Dioscorea dumetorum (Pax), in chloroquine phosphate tablet formulations in comparison with official corn starch.

Method: Compressional properties were analyzed using density measurements and compression equations of Heckel and Kawakita. The mechanical properties of the tablets were assessed using the crushing strength and friability of the tablets, while drug release properties of the tablets were assessed using disintegration and dissolution times.

Results: Tablet formulations containing trifoliate yam starch exhibited faster onset and higher amount of plastic deformation during compression than those containing corn starch. The crushing strength, disintegration and dissolution times of the tablets increased with binder concentration while friability values decreased. Trifoliate yam starch produced tablets with stronger mechanical properties and longer disintegration and dissolution times than those containing corn starch.

Conclusion: Trifoliate yam starch would be a better alternative to corn starch in producing uncoated tablets for which high bond strength is essential.

Keywords: Trifoliate yam starch, corn starch, binding agent, compression, Heckel equation, Kawakita equation, mechanical properties, drug release.

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INTRODUCTION

A survey of the literature shows that the usefulness of starches from various botanical sources as pharmaceutical excipients has formed a subject of interesting study for close to four decades ¹⁻⁵. Starches are widely available and have been very useful in tablet production due to their inertness, cheapness and utilization as fillers, binders, disintegrants and glidants ^{6,7}.

Many starches obtained from different food crops have shown enough potential as excipients in tablet formulations to stimulate further research and development efforts. In this regard, a lot of efforts have been expended to develop locally produced starches as binders and disintegrants⁸. Nasipuri evaluated the use of *Dioscorea rotundata* as a binder and disintegrant in tablet formulation¹ and Itiola also investigated the compressional properties of this particular starch ⁹. However, little work has been done to evaluate the effects of trifoliate yam starch obtained from *Dioscorea dumetorum* (Pax) on the compressional, mechanical and release properties of tablet formulations.

The Heckel equation is widely used for relating the relative density, D, of a powder bed during compression to the applied pressure, P ^{10, 11}. It is written as:

$$\ln\left[\frac{1}{(1-D)}\right] = KP + A$$
[1]

where K and A are constants.

The Heckel equation is a sensitive tool to study the compressibility of materials. It describes the relationship of the compact density to the applied pressure. The slope of the straight line portion, K, is the reciprocal of the mean yield pressure, P_y , of the material. The intercept of the extrapolated linear portion, A, is a function of the original compact volume.

From the value of A, the relative Density (D_A) can be calculated using the following equation.

$$D_A = 1 - e^{-A}$$
 [2]

The relative density of the powder bed at the point when the applied pressure equals zero, D_{O} , is used to describe the initial rearrangement phase of densification as a result of die filling

and this is obtained from the ratio of the loose density to the particle density. The relative Density, D_B , describes the phase of rearrangement of particles during the initial stages of compression. The extent of rearrangement phase depends on the theoretical point of densification at which deformation of particles begins.

Thus,
$$D_B = D_A - D_0$$
 [3]

The Kawakita equation¹³ is used to study of powder compression using the degree of volume reduction (C) and is written as:

$$C = (Vo - Vp)/Vo = abP/(1+bP)$$
 [4]

The equation in practice can be rearranged as:

$$P/C = (P/a) + (1/ab)$$
 [5]

in which V_o is the powder's initial bulk volume and V_p is the bulk volume after compression. The constant, 'a' is the material's minimum porosity before compression while the constant 'b' relates to the material's plasticity. The reciprocal of b defines a pressure term P_k , which is the pressure required to reduce the powder bed by 50% $^{14,\,15}$.

Thus, the present study was designed to evaluate the effects of trifoliate yam starch as a binder in a chloroquine phosphate tablet formulation in comparison to official corn starch BP grade.

Chloroquine phosphate was chosen for the work because of its poor tableting properties and hence requires a binder among other excipients to form satisfactory tablets.

MATERIALS AND METHODS

Materials

The materials used were chloroquine phosphate powder (product of People's Republic of China, made to the specification of BP 1988, Bentos Pharmaceutical supplied by and Products Ltd., Nigeria), corn starch BP (Lot 69833 supplied by Bentos Pharmaceutical Products Ltd., Nigeria), Lactose B. P (DVM Veghel, Holland) and Trifoliate (Wild) yam starch obtained from the tubers of Dioscorea dumetorum (Pax). The experimental starch was prepared in a University of Ibadan laboratory.

The description of the preparation and purification of the starches have been given elsewhere ¹². The particle density of granules was determined by the pycnometer method using xylene as the displacement fluid

Preparation of granules

250g batches of a basic formulation comprising of chloroquine (60%w/w), Lactose (30% w/w) and corn - starch (10% w/w) were dry mixed for about five minutes in a Kenwood planetary mixer. The mixture was then moistened with appropriate amount of pastes of the binding agent (Wild yam, *Dioscorea dumetorum* starch or and corn starch) to produce samples containing 2.5, 5.0, 7.5 and 10.0%w/w of the binders.

Massing was continued for about five minutes and the wet masses were granulated by passing them manually through a N0 12 mesh sieve (1,400 μ m). The granules were dried in a hot air oven for 24hours at 60° C and then resieved through a N0 16 mesh sieve (1,000 μ m), before they were stored in air - tight containers.

Determination of pre-compression pressure

The bulk density of each formulation at zero pressure (loose density) was determined by pouring the granules into a 50ml glass measuring cylinder with a diameter of 24mm through a funnel at an angle of 45° . Determinations were made in triplicate. The relative density D_{\circ} of each formulation was obtained from the ratio of the loose density to its particle density.

Preparation of tablets

A Carver hydraulic hand press (Model C, Carver Inc, Menomonee Falls, Wisconsin, U. S. A), fitted with a pressure gauge reading up to 2.5 metric tonnes was used.

Granules of size fraction $500 - 1,000 \mu m$ were used to prepare $400 mg \pm 10 mg$ tablets using a 10.5 mm diameter die in combination with flat faced upper and lower punches. Before each compression, the punches and die were lubricated by brushing with 2% w/v dispersion of magnesium stearate in ethanol - ether (1:1). After ejection, the tablets were stored over silica gel for 24 hr before tablet properties were

determined, to allow for elastic recovery and hardening and prevent false low yield values.

The weights (w) of the tablets were accurately determined at room temperature to within \pm 1mg while the diameter and thickness of the tablets were accurately measured to within \pm 0.01mm .The relative densities D, of the tablets were calculated from the equation:

$$D = \frac{w}{V_t \cdot \rho_s}$$
 [6]

where V_t is the volume of tablet (cm³) and ρ_s is the particle density of the solid material (g/cm³).

Crushing strength and friability tests

Ten tablets from each formulation were tested for diametrical crushing test using the Erweka TBH 28 hardness tester (Apparatebau, GMBH, Germany). Measurements were made in triplicate on individual tablets and the crushing strength results were accepted only if the samples split cleanly into two halves. The friability of the tablets was also determined using the Veego tablet friability apparatus (Veego Scientific Devices, Mumbai, India) at a speed of 25rpm for 4minutes.

Disintegration test

The disintegration times of the tablets were determined in distilled water at $37^{\circ} \pm 0.5^{\circ}$ C using the Apex disintegration testing Apparatus (Apex Construction Ltd; Northflect Gravescent and Dartford, Kent,U.K).

Tablets were placed on the wire mesh just above the surface of the water in the tube and the apparatus was started simultaneously with a stop clock. The tablets were kept in contact with distilled water contained in the tube. The time taken for all the tablets to disintegrate and go through the wire mesh was recorded. Determinations were made in triplicate.

Dissolution test

The dissolution rate of the tablets was determined in distilled water using the Rotating Basket (USP Apparatus I) method. Each tablet was placed in a cylindrical basket of stainless wire mesh attached to a variable speed drive mechanism and suspended in a glass vessel

TABLE 1: Parameters Obtained From Density Measurements and Heckel And Kawakita Plots

Starch	Binder conc. (% w/w)	D _o	Heckel Plots			Kawakita Plots	
			P _y (MN/m ²)	D _A	D _B	P _k (MN/m)	D _i
	0.0	0.276	95.56	0.863	0.587	3.212	0.424
Trifoliate yam	2.5	0.346	114.21	0.772	0.426	2.661	0.410
	5.0	0.387	111.12	0.802	0.415	2.583	0.403
	7.5	0.392	96.91	0.800	0.408	2.449	0.397
	10.0	0.357	90.81	0.783	0.401	2.385	0.362
Corn Starch	2.5	0.284	142.86	0.830	0.546	2.889	0.339
	5.0	0.281	125.10	0.823	0.542	2.770	0.321
	7.5	0.278	121.41	0.817	0.539	2.685	0.318
	10.0	0.261	97.62	0.793	0.532	2.496	0.299

containing 900mls of distilled water which was immersed in a water bath set at $37^{\circ}\pm0.5^{\circ}$ C.

The apparatus was set to rotate at 100rpm and was started simultaneously with a stop clock. 5ml samples of the dissolution medium was removed at designated intervals and replaced with an equal volume of fresh sample of dissolution medium. The absorbance of the removed samples was measured and the total concentration of drug in each sample was determined using a UV spectrophotometer (SP6-450 UV/VIS spectrophotometer, Pye Unicam, Middlesex, England)

Statistical analysis

Statistical analysis was done to compare the effect of trifoliate yam starch and corn starch on tablet properties using the *t*-test. At 95% confidence interval, *p* value lower or equal to 0.05 was considered the limit of significance.

RESULTS AND DISCUSSION

Fig. 1 shows representative Heckel plots phosphate for chloroquine formulations containing 5%w/w binder. The mean yield pressure, P_v, was calculated from the regions of the plots showing linearity with correlation coefficient of \geq 0.990 for all formulations (generally between 56.62 and 198.16MNm-2). The intercept A was determined from the extrapolation of the region used for the determination of P_v. The intercept represented the point at which a coherent or intact tablet was just formed during compression. The values of D_A and D_B were calculated from Eqn. 2 and 3 respectively. The values of P_Y, D_O, D_A, and D_B for the formulations are presented in Table 1.

The values of $D_{\it o}$ for the various formulations increased with binder concentration, implying that the initial packing of the formulation as a result of die filling increased with increase in binder content. These values were found to be higher for formulations containing trifoliate yam starch.

Table 2. Crushing strength, friability and crushing strength-friability ratio (csfr) for chloroquine phosphate tablets at relative density 0.90

Starch	Binder conc. (% w/w)	Crushing strength (N)	Friability (%)	CSFR
	0.0	34.31 ± 2.10	3.83 ± 0.04	8.95
Trifoliate yam	2.5	73.50 ± 1.22	2.37 ± 0.02	31.01
	5.0	78.41 ± 1.02	1.33 ± 0.03	58.95
	7.5	83.33 ± 2.13	0.83 ± 0.02	100.36
	10.0	88.21 ± 1.03	0.63 ± 0.03	140.00
Corn Starch	2.5	53.92 ± 1.21	2.41 ± 0.06	22.37
	5.0	56.41 ± 2.01	1.40 ± 0.02	40.29
	7.5	58.82 ± 2.14	0.96 ± 0.05	61.25
	10.0	44.10 ± 1.17	0.78 ± 0.02	56.54

The mean yield pressure P_y is inversely related to the ability of a material to deform plastically when compressed. The values of P_y decreased with increase in binder concentration, with formulations containing trifoliate yam starch having lower values compared to corn starch. This implies that the onset of plastic deformation in the formulations containing trifoliate yam starch was faster than those containing corn starch.

Fig. 2 shows representative Kawakita plots for chloroquine phosphate formulations containing 5% w/w binders. A linear relationship was obtained at all compression pressures employed with a correlation coefficient ≥ 0.999 for all formulations. Values of a and ab were obtained from the slope and intercept of the plots, respectively. Values of 1-a give the initial

relative density, D_I , of the formulations, while P_k values were obtained from the reciprocal of values of b. Values of P_k and D_I are included in Table I.

 D_{l} values decreased with The concentration of starch binder in all formulations, with formulations containing trifoliate vam starch having lower values than corn starch formulations. The D_I values are also observed to be higher than the corresponding values of loose initial relative density Do. Hence, these results suggest that D_I values provide a measure of the packed initial relative density of the formulations on application of small pressure or tapping in contrast to that of Do, which provide a measure of loose initial relative density due solely to die filling ¹⁷.

Table 3. Disintegration and dissolution characteristics of chloroquine phosphate tablets At relative density 0.90 (mean \pm sd, n=4)

Starch	Binder conc. (% w/w)	D (min)	t ₈₀ (min)	t ₁ (min)	k ₁	k ₂
	0.0	3.83 ± 1.01	38.25 ± 0.95	34.14 ± 1.05	0.044 ± 0.012	0.134 ± 0.031
Trifoliate yam	2.5	5.03 ± 0.22	44.12 ± 1.25	31.25 ± 0.24	0.054 ± 0.001	0.237 ± 0.021
	5.0	7.02 ± 0.15	46.28 ± 0.85	33.62 ± 0.15	0.052 ± 0.014	0.126 ±0.014
	7.5	8.53 ± 1.02	58.03± 3.21	41.66 ± 0.13	0.041 ± 0.003	0.085 ± 0.002
	10.0	9.04 ± 0.16	61.52± 2.47	46.72 ± 0.52	0.029 ± 0.008	0.063 ± 0.120
Corn Starch	2.5	5.01 ± 0.14	40.14± 0.27	29.42 ± 0.14	0.036 ± 0.001	0.123 ± 0.005
	5.0	6.55 ± 0.75	42.18 ± 1.19	31.86 ± 0.75	0.033 ± 0.003	0.103 ± 0.001
	7.5	7.02 ± 0.45	45.63± 2.02	36.07 ± 0.98	0.029 ± 0.015	0.062 ± 0.210
	10.0	9.51 ± 0.18	47.86± 1.14	38.22 ± 0.17	0.018 ± 0.001	0.059 ± 0.004

Values of Pk, which are an inverse measure of the amount of plastic deformation occurring during the compression process 17, also decreased with starch concentration. Formulations containing Trofoliate yam starch had lower values than those containing corn starch. This implies that formulations containing corn starch exhibited a lower degree of total plastic deformation during the compression would process. Hence. it appear formulations containing trifoliate yam starch exhibited a faster onset of plastic deformation during compression as indicated by the low P_v values, and also exhibited a higher degree of plastic deformation during the compression process.

There were no clear cut patterns to the variation of the values of D_0 , D_B and D_A with binder concentration. However, the values of D_O (packing during die filling) for formulations containing yam starch were significantly (P<0.001) higher than for those containing corn starch. While, the values of D_B (densification at low pressures) for formulations containing corn starch were significantly (P<0.001) higher than those of formulations containing yam starch. In addition, the total degree of packing (DA) achieved was significantly (P<0.05) higher form formulations containing corn starch. formulations containing corn starch exhibited more packing of particles before a coherent tablet was formed during compression.

The mechanical properties of the tablet formulations were assessed by the crushing strength and friability of the tablets. While

crushing strength indicates the strength of the tablet, friability values provide a measure of tablet weakness. Table 2 presents values of strength friability and formulations at a relative density of 0.90, which is representative of commercial tablets. There increase in crushing strength with corresponding decrease in friability values with binder concentration for all formulations. It has been established that the presence of high concentration of plasto-elastic binding agent leads to an increase in plastic deformation of the formulation and consequently to the formation of more solid bonds with increase in tablet strength and resistance to fracture and abrasion. Formulations containing the experimental starch had higher crushing strength values which could be due to the lower Pk values which indicate plastic deformation greater total during compression.

The crushing strength-friability ratio (CSFR) also provides a parameter for measuring tablet strength 17 . Generally, the higher the CSFR value, the stronger the tablet. The CSFR values for all formulations are included in Table 2. An increase was observed for the tablets with increase in binder concentration, with tablets containing trifoliate yam starch showing significantly (p<0.05) higher values than tablets containing corn starch.

The disintegration time values for the tablets at relative density of 0.90 are presented in Table 3. An increase was observed in disintegration time with increase in binder concentration for all formulations, although there

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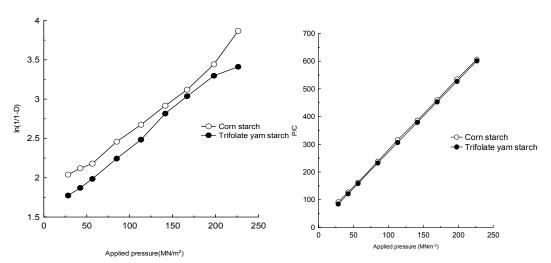


Fig 1.: Heckel plots for chloroquine phosphate tablets containing 5%w/w starch as binder

Fig. 2: Kawakita plots for chloroquine phosphate tablets containing 5%w/w starch as binder

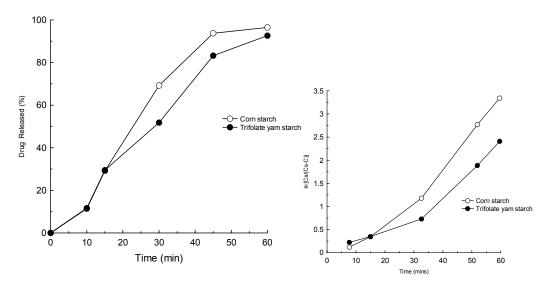


Figure 3: Dissolution plot for chloroquine phosphate released vs. time for tablets containing 5%w/w binder

Figure 4: In [Cs/(Cs-c)] vs. time for chloroquine phophate tablets containing 5%w/w starch as binder

were no significant (p>0.05) differences in disintegration time between the formulations. However, all tablets passed the British Pharmacopoeia specifications for disintegration of uncoated tablets within 15minutes.

Fig. 3 shows representative plots of the amount of chloroquine phosphate released against time for tablets containing 5% w/w binder. The values of t_{80} (time taken for 80% of the drug to be released) were calculated. These

values for all formulations at a relative density of 0.90 are presented in Table 3. The t_{80} values increased with binder concentration for all tablets with trifoliate yam starch formulations showing higher values than those containing corn starch.

The data obtained was further subjected to Kitazawa et al. ¹⁸ analysis which involves the integrated form of the Noyes-Whitney equation ¹⁹ written as

$$\ln \left[\frac{Cs}{(Cs - C)} \right] = kt \tag{7}$$

where C_s is the concentration of the solute at saturation, C is the concentration at time t, and k is dissolution rate constant. Values of $\ln \left[C_s / (C_s - C) \right]$ were plotted versus t and shown for tablets containing 5% w/w of binder in Figure 4

The Kitazawa plots generally showed two straight regression lines of slopes K_1 and K_2 . The time at which the lines intersect is denoted t_1 . Values of k_1 , k_2 and t_1 for all samples at relative density, D of 0.90 are presented in Table 3. The Table shows k_1 to be lower than k_2 implying that the dissolution rate of the drug was faster after t_1 . It would appear that changes in surface area of the dissolving particles brought about by the disintegration and de-aggregation of the tablets were manifested in the substantial increase in dissolution rate after t_1 . Values of t_1 , k_1 and k_2 for formulations containing trifoliate yam starch were higher than those for formulations containing corn starch.

CONCLUSION

The results of the present study show that trifoliate yam starch as a binder in chloroquine phosphate tablets provides faster onset and higher amount of total plastic deformation under compression pressure than corn starch. Trifoliate yam starch also produced tablets with stronger mechanical properties and longer disintegration and dissolution times than corn starch BP. The results suggest that trifoliate yam could be useful as a binding agent when a requirement of high mechanical strength is more essential.

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